NEMA Standards Publication No. CP 1-1988 (R1992, R2000)

Shunt Capacitors

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National Electrical Manufacturers Association
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Foreword

These requirements for shunt capacitors are issued by NEMA, reflecting the latest standards affecting these products. They are made available as a guide for the manufacturer and to assist the purchaser in selecting and obtaining a suitable product. This Standards Publication applies to capacitors designed for shunt connections to alternating-current power transmission and distribution systems operating at frequencies of 50 or 60 Hz and below. The use of these standards is at the option of the individual manufacturer and the purchaser. It is anticipated that those who utilize them will derive benefit from the advantages of functional interchangeability. To assure a meaningful publication, copies were sent during the draft stage to a number of individuals and organizations in the public and private sector having an interest in or responsibility for the purchase, testing, application, use, or inspection of this product category. The resulting comments and suggestions provided a vital user and general interest input to final NEMA approval and resulted in a number of substantive changes being made in this publication.

This Standards Publication duplicates the requirements of the American National Standard for Shunt Power Capacitors ANSI C55.1. Additional requirements are also covered, but they are not intended to conflict with ANSI C55.1.

These standards are periodically reviewed by the Capacitor Section of NEMA for any revisions necessary to keep them up to date with advancing technology. As future major revisions to this publication are proposed, it is intended to offer to both individuals and organizations in the public and private sector a further opportunity to participate in the development of this publication.

Proposed or recommended revisions should be submitted to:

Manager, Engineering Department
National Electrical Manufacturers Association
2101 L Street, N. W.
Washington, D. C. 20037

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Scope

This standard applies to capacitors rated 216V or higher, 5 kV or more, and designed for shunt connection to alternating current transmission and distribution systems operating at a nominal frequency of 50 or 60 Hz.

The values stated in U.S. customary units are to be regarded as the standard.

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SHUNT CAPACITORS

SECTION 1
REFERENCED STANDARDS AND DEFINITIONS

1.1 REFERENCED STANDARDS

American National Standards Institute
1430 Broadway
New York, NY 10018

ANSI C55.1-1980 (IEEE 18-1980)	*Shunt Power Capacitors*
ANSI/IEEE 100-1984	*Dictionary of Electrical and Electronic Terms*
ANSI C37.30-1971 (IEEE 324-1971)	*Definitions and Requirements for High Voltage Air Switches, Insulators, and Bus Supports*
ANSI C76.1-1976 (IEEE 21-1976)	*General Requirements and Test Procedures for Outdoor Apparatus Bushings, Part 1*

National Electrical Manufacturers Association
2101 L Street, N.W.
Washington, DC 20037

ICS 2-1983	*Industrial Control Devices, Controllers, and Assemblies*
107-1987	*Methods of Measurement of Radio Influence Voltage (RIV) of High Voltage Apparatus*

National Fire Protection Association
Batterymarch Park
Quincy, MA 02269

NFPA 70-1987	*National Electrical Code*

1.2 DEFINITIONS

Unless listed below, definitions shall be as shown in ANSI C55.1-1980 or in ANSI/IEEE 100-1984.

Ambient temperature is the temperature of the surrounding cooling medium, usually air, which comes into contact with the heated parts of the apparatus.

Capacitor is an assembly of a dielectric and electrodes in a container with the terminals brought out, the primary purpose of which is to introduce capacitance into an electric circuit.

Capacitor bank is two or more capacitors in one location, either under one control or separate controls.

Capacitor bus is the conductor that serves as a common connection between the connectors from the capacitors and the line.

Capacitor connectors are devices used to connect capacitors to the capacitor bus.

Capacitor equipment is a complete assembly of capacitors, including accessories such as buses, connectors, dischargers, fuses, switching devices, and controls, suitable for connection to a circuit.

Capacitor hanger is an open framework for mounting one or more capacitors from crossarms, poles, walls, or ceilings.

Connection diagram is a diagram that shows the connections of an installation or its component devices, controllers, and equipment. It covers internal or external connections, or both, and shall contain such detail as is needed to make or trace connections that are involved.

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A connection diagram excludes mechanical drawings, such as wiring templates, wiring assemblies, and cable assemblies.

The connection diagram shows the general physical arrangement of devices and device elements with accessory items such as terminal blocks, resistors, and such.

Discharger is a device, connected across the terminal of a capacitor or buses or built into the capacitor, which reduces the residual voltage after the capacitor is disconnected from the line.

Enclosed capacitor is a capacitor with enclosed terminals which is provided with means for connection to a conduit.

Floating neutral is a one whose voltage to ground is free to vary when circuit conditions change.

Fused capacitor is a capacitor with fuses mounted either on its terminals, inside a terminal enclosure, or inside the capacitor container.

Illustrative diagram is a diagram that principally shows the operating principle of a device or a group of devices without necessarily showing actual connections or circuits. Illustrative diagrams use pictures or symbols to illustrate or represent devices or their elements.

Illustrative diagrams show electric, hydraulic, pneumatic, and combinations systems. They are applicable chiefly to instruction books, descriptive folders, or other mediums whose purpose is to explain or instruct.

Indoor, as a prefix, indicates that the apparatus is suitable for indoor service only.

Metal-enclosed or housed equipment is capacitor equipment enclosed in a metal enclosure or metal house to prevent accidental contact with live parts.

Non-enclosed capacitor is a capacitor that is not provided with an individual enclosure for the terminals.

One-line (or single-line) diagram is a diagram that, by means of single lines and simplified symbols, indicates the route and component devices, or parts of an electric circuit, or system of circuits. Physical relationships are usually disregarded. One-line (or single-line) diagrams are useful in showing the overall relations between component devices and circuit, and between circuits.

Outdoor, as a prefix, indicates that the apparatus is suitable for outdoor service. A capacitor or equipment is designed as dust-, weather-, and such, when so constructed, protected, or treated that its successful operation is not interfered with when subjected to the specified material or condition.

Rack is a structure that supports the capacitors.

Rack equipment is capacitor equipment without enclosing plates or screens.

Schematic or elementary diagram is a diagram which shows all circuits and device elements of an equipment and its associated apparatus or any clearly defined functional portion thereof. Such a diagram emphasizes the device elements of a circuit and their functions as distinguished from the physical arrangement of the conductors, devices, or device elements of a circuit system.

Var is the unit of reactive power and is the product of the root-mean-square (rms) voltage, the rms current, and the sine of the angle between. Since capacitor current leads its voltage by 90 degrees, the sine is unity and the reactive power is the voltage times capacitor current.

To emphasize the device elements and show their functional relationships and sequence, physical relationships of devices and device elements are disregarded. Circuits are drawn in the most direct possible line between and perpendicular to parallel lines representing opposite polarities of voltage sources, and circuits that function inherently in a definite sequence are arranged to indicate that sequence.

Schematic or elementary diagrams are used to indicate electrical relationships of circuits and device elements.

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SECTION 2
SERVICE CONDITIONS

2.1 GENERAL

For additional information on service conditions, see Section 6.

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2.2 ALTITUDE

Capacitors shall be suitable for operation at altitudes not exceeding 6,000 feet (1,800 meters) above sea level (See 4.7).

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Although the capacitor requires no derating up to 6,000 feet (1,800 meters), other insulation in an equipment may require derating above 1,000 meters as specified in ANSI C37.30.

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2.3 AMBIENT TEMPERATURE

Capacitors and equipment shall be suitable for switched or continuous operation outdoors with unrestricted ventilation when operated within the limits specified in Table 2-1 and when installed in accordance with 2.5.

2.3.1 Maximum Ambient Temperature

Table 2-1
Ambient Air Temperature
Degrees C

Mounting-Arrangement	Average*	24-hour NormalAnnual +
Isolated capacitor	46	35
Single row of capacitators	46	35
Multiple row and tiers of capacitors	40	25
Metal-enclosed or housed equipments	40	25

*The 24-hour arithmetic average of hourly readings during the hottest day expected at the location.

+As defined in the reports of the U.S. Weather Bureau.

2.3.2 Minimum Ambient Temperature

The minimum allowable ambient temperature shall be –40°C.

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For operation at ambient temperatures other than those listed in Table 2-1 or in indoor locations with restricted ventilation, see 6.4.

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2.4 DETERMINATION OF AMBIENT TEMPERATURE

The ambient temperature shall be determined by taking the average of the readings of three thermometers placed as follows:

1. One level with the top of the equipment or, where included, with the top of the uppermost outlet ventilation opening;
2. One 12 inches above the bottom of the equipment or, where included, level with the center of the lowest inlet ventilation opening; and
3. One midway between the two above positions.

All three thermometers shall be placed 12 inches away horizontally from the equipment and in locations unaffected by drafts caused by the equipment or by other apparatus. These thermometers shall be immersed in a suitable liquid, such as oil, in a heavy metal cup when the ambient temperature is subject to such variations that errors in taking the temperature might result. Also, these thermometers shall be shielded from direct radiation from the sun or other heated surfaces.

NEMA Standard 11-17-1988.

2.5 MOUNTING AND INSTALLATION OF CAPACITORS AND EQUIPMENT

2.5.1 Position

Capacitors shall be designed for normal mounting in a vertical or horizontal position with the entrance bushings at the top, except where other mountings are specifically recommended by the manufacturer.

2.5.2 Arrangements

Racks and housings shall have provision for mounting individual capacitors in one, two, or three tiers, with no more than two rows of capacitors per tier. Enclosures having one row of capacitors per tier shall be accessible from one side only; those having two rows per tier shall be accessible from two opposite sides.

The horizontal spacing, center to center, between capacitors in a metal-enclosed equipment shall be sufficient to provide for the circulation of cooling air and to provide ample clearances between live parts during normal operation or with a short-circuited individual capacitor and a blown fuse.

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The bottom tier of capacitors in all racks or housings shall be sufficiently above the level of the base to permit unrestricted ventilation.

The top of indoor capacitor equipment shall be sufficiently below the ceiling to permit unrestricted ventilation and to avoid pocketing the equipment in dead air.

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2.5.3 Unusual Installation Requirements

Unusual conditions may require a variation from the installations described in 2.5.1 and 2.5.2 and should be brought to the attention of the manufacturer for special consideration and recommendations. Among such unusual conditions are:

1. Limited floor space requiring:
   a. More than three tiers;
   b. More than two rows of capacitors per tier;
   c. Restricted aisle space for accessibility; and/or
   d. Limited physical entrance requirements for installation.
2. Rooms not having normal ventilation, rooms containing other apparatus radiating heat, or rooms with unusual configurations or partitions causing hot air pockets;
3. Unusual dust or other conditions causing the partial obstruction of ventilation;
4. Severe vibration of the foundation on which the capacitor is supported;
5. Open supporting foundation requiring enclosed or screened bottom for capacitor equipments; and/or
6. Unusual lead entrance requirements.

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2.6 WORKING VOLTAGES

Capacitors shall be suitable for use on line-to-line circuit voltages corresponding to their ratings and for use on line-to-neutral voltages corresponding to their ratings on solidly grounded neutral circuits.

Capacitors shall be suitable for operation at a terminal-to-terminal voltage (rms including harmonics) of 110 percent of rated voltage (exclusive of transients).

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2.7 MAXIMUM WORKING VOLTAGE

The maximum continuous working voltage of capacitors shall be 110 percent of the rated voltage rms provided that the crest voltage including all harmonics does not exceed $1.2 \times \sqrt{2}$ times rated voltage.

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It is recognized that during switching, sudden loss of load and the like, the voltage of a system may rise momentarily above the maximum working voltage, but there is no provision for this contingency other than the factor of safety introduced by the test voltage (see 6.3).

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2.8 MAXIMUM REACTIVE KVAR

Capacitors shall be suitable for continuous operation at 135 percent of rated reactive power. This maximum reactive power shall include the following factors, the combined effects of which shall not exceed 135 percent:

1. Reactive power due to voltage in excess of nameplate rating at fundamental frequency but within the permissible voltage limitations described in 2.7;
2. Reactive power due to harmonic voltages superimposed on the fundamental frequency; and
3. Reactive power in excess of nameplate rating due to manufacturing tolerance within the limits specified in 5.11.

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2.9 UNUSUAL SERVICE CONDITIONS

Unusual service conditions may require special construction or operation, and these should be brought to the attention of those responsible for the manufacture and application of the equipment. Among such unusual conditions are:

1. Operation at altitudes above 6,000 feet (1,800 meters) above sea level (see 4.8);
2. Ambient temperatures higher or lower than those specified in 2.3 or exposure to sudden changes in temperature or to radiated heat from surfaces whose temperature is higher than the applicable ambient temperature. Excessive ambient temperatures may be encountered in rooms not having normal ventilation or with unusual configurations or partitions causing hot air pockets, or in rooms containing other heat-producing apparatus (see 6.4);
3. Exposure to salt air, damaging fumes or vapors, steam, excessive moisture, or dripping water;
4. Exposure to excessive, abrasive, or conductive dust;
5. Exposure to explosive mixtures of dust or gases;
6. Exposure to severe weather conditions;
7. Exposure to abnormal vibration, shocks, or tilting;
8. Unusual transportation or storage conditions;

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9. Unusual space limitations;
10. Unusual insulation or voltage requirements;
11. Unusual operating duty, frequency of operation or difficulty of maintenance;
12. Operation at unstable control voltages;
13. Unusual wave form distortion or harmonics causing excessive current, voltage, or kvar loading (see 6.3 and 6.5); and/or
14. Any other unusual or special operating requirements.

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SECTION 3
RATING STANDARDS

3.1 BASIS OF RATING

Capacitors shall be rated in kvar, rms voltage (terminal-to-terminal), frequency, number of phases, and terminals-to-case (ground) basic impulse level (see Table 3-1).

Capacitors shall give not less than the rated reactive power at rated sinusoidal voltage and frequency, and not more than 115 percent of this value, measured at 25°C uniform case and internal temperature.

NEMA Standard 11-17-1988.

3.2 FREQUENCY

The capacitors shall be suitable for operation at frequencies of 50 or 60 Hz and below.

NEMA Standard 11-17-1988.

Capacitors are not intended for operation at predominant frequencies above rated frequency. Capacitors may be used where higher rated frequency components are present, provided these components do not result in excessive operating current, based on rated kvar, frequency and rms voltage and provided the operating kvar does not exceed the value given in 2.8 (see 6.5).

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3.3 VOLTAGE AND KVAR RATINGS FOR INDOOR CAPACITORS

The rms voltage and kvar ratings for indoor capacitors rated at 60 Hz shall be in accordance with Table 3-2.

NEMA Standard 11-17-1988.

Table 3-2
Indoor Capacitor Ratings

Volts RMS	KVAR	Number of Phases
216	2.5, 5, 7½, 10, 15, 20, and 25	1 and 3
240	2.5, 5, 7½, 10, 15, 20 ,25, and 50	1 and 3
480	5, 10, 15, 20, 25, 35, 50, 60, and 100	1 and 3
600	5, 10, 15, 20, 25, 35, 50, 60, and 100	1 and 3

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Table 3-1
Voltage and KVAR Ratings for 60 Hz Capacitors

Volts, RMS (Terminal-to-Terminal)	KVAR	Number of Phases	BIL KV (†)
216	5, 7½, 13⅓, 20, and 25	1 and 3	30‡
240	2.5, 5, 7½, 10, 15, 20, 25, and 50	1 and 3	30‡
480	5, 10, 15, 20, 25, 35, 50, 60, and 100	1 and 3	30‡
600	5, 10, 15, 20, 25, 35, 50, 60, and 100	1 and 3	30‡
2400	50, 100, 150, and 200	1	75
2770	50, 100, 150, and 200	1	75
4160	50, 100, 150, and 200	1	75
4800	50, 100, 150, and 200	1	75
6640	50, 100, 150, 200, 300, and 400	1	95
7200	50, 100, 150, 200, 300, and 400	1	95
7620	50, 100, 150, 200, 300, and 400	1	95
7960	50, 100, 150, 200, 300, and 400	1	95
8320	50, 100, 150, 200, 300, and 400	1	95
9540	50, 100, 150, 200, 300, and 400	1	95
9960	50, 100, 150, 200, 300, and 400	1	95
11400	50, 100, 150, 200, 300, and 400	1	95
12470	50, 100, 150, 200, 300, and 400	1	95
13280	50, 100, 150, 200, 300, and 400	1	95 and 125
13800	50, 100, 150, 200, 300, and 400	1	95 and 125
14400	50, 100, 150, 200, 300, and 400	1	95 and 125
15125	50, 100, 150, 200, 300, and 400	1	125
19920	100, 150, 200, 300, and 400	1	125
19920*	100, 150, 200, 300, and 400	1	125
20800*	100, 150, 200, 300, and 400	1	150 and 200
21600*	100, 150, 200, 300, and 400	1	150 and 200
22800*	100, 150, 200, 300, and 400	1	150 and 200
23800*	100, 150, 200, 300, and 400	1	150 and 200
24940*	100, 150, 200, 300, and 400	1	150 and 200
4160GrdY/2400	300 and 400	3	75
4800GrdY/2770	300 and 400	3	75
7200GrdY/4160	300 and 400	3	75
8320GrdY/4800	300 and 400	3	75
12470GrdY/7200	300 and 400	3	95
13200GrdY/7620	300 and 400	3	95
13800GrdY/7960	300 and 400	3	95
14400GrdY/8320	300 and 400	3	95

(†) See 5.6 *1 bushing ‡Not applicable to indoor rating

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SECTION 4
MANUFACTURING STANDARDS

4.1 CAPACITOR TERMINALS

Single-phase capacitors shall have one or two insulated terminals. Three-phase capacitors shall have three or four insulated terminals.

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4.2 PROVISION FOR MAKING CONNECTIONS TO CAPACITOR EQUIPMENT

A bushing, cable, or conduit entrance shall be provided for outdoor metal-enclosed capacitor equipment rated above 600 V.

NEMA Standard 11-17-1988.

4.3 DISCHARGE DEVICES

Capacitors to be installed under the conditions covered by the *National Electrical Code* shall be provided with a means for reducing the residual voltage in accordance with the requirements. Capacitors connected directly to other electric equipment that provides a discharge path without having a disconnecting switch, fuse, or cutout interposed shall be considered properly discharged. The discharge circuit shall be permanently connected to the terminals of the capacitor or capacitor bank. Manual or automatic means for switching or connecting the discharge circuit shall not be used.

Capacitors not subject to the requirements of the *National Electrical Code* shall be provided with a means for reducing the residual voltage to 50 V or less within the following time limits specified in Table 4-1 after the capacitor is disconnected from the source of supply.

Capacitor equipment which is automatically switched shall be provided with a discharge means for reducing the residual voltage to 50 V or less between one switching operation and the next, unless otherwise recommended by the manufacturer.

NEMA Standard 11-17-1988.

Table 4-1
Discharge Time Limits

Range of Capacitor Voltage Ratings (Terminal-to-Terminal) Volts, rms	Maximum Time Limit
600 volts or less	1 minute
Over 600 volts	5 minutes

The internal discharge device provided in capacitors should not be considered as a substitute for the recommended practice of manually discharging the residual stored charge before working on capacitors. The use of a discharge device is intended to supplement rather than displace the short-circuiting of a capacitor before handling.

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4.4 DIMENSIONS

4.4.1 Mounting Hole Spacings

The mounting hole spacings of capacitors rated 5 to 400 kvar (single phase) shall be 15 5/8 inches ± 1/16 inch (397.0 mm ± 1.6 mm) between centers of 7/16 inch (11.1 mm) minimum diameter holes. Three phase cantilever mounted capacitors shall accommodate 5/8 inch (15.9 mm) mounting bolts at 18 inches ± 1/16 inch (457.2 mm ± 1.6 mm) between centers.

NEMA Standard 11-17-1988.

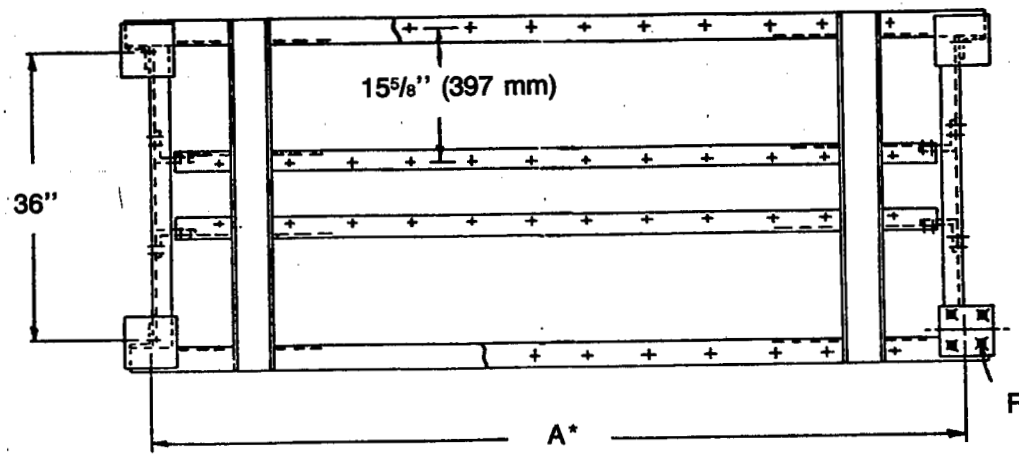
4.4.2 Upright Non-Enclosed Substation Equipment

Upright non-enclosed substation equipment using 50 kvar, 100 kvar, 150 kvar, 200 kvar, 300 kvar, and 400 kvar single-phase capacitors shall be as shown in Figure 4-1.

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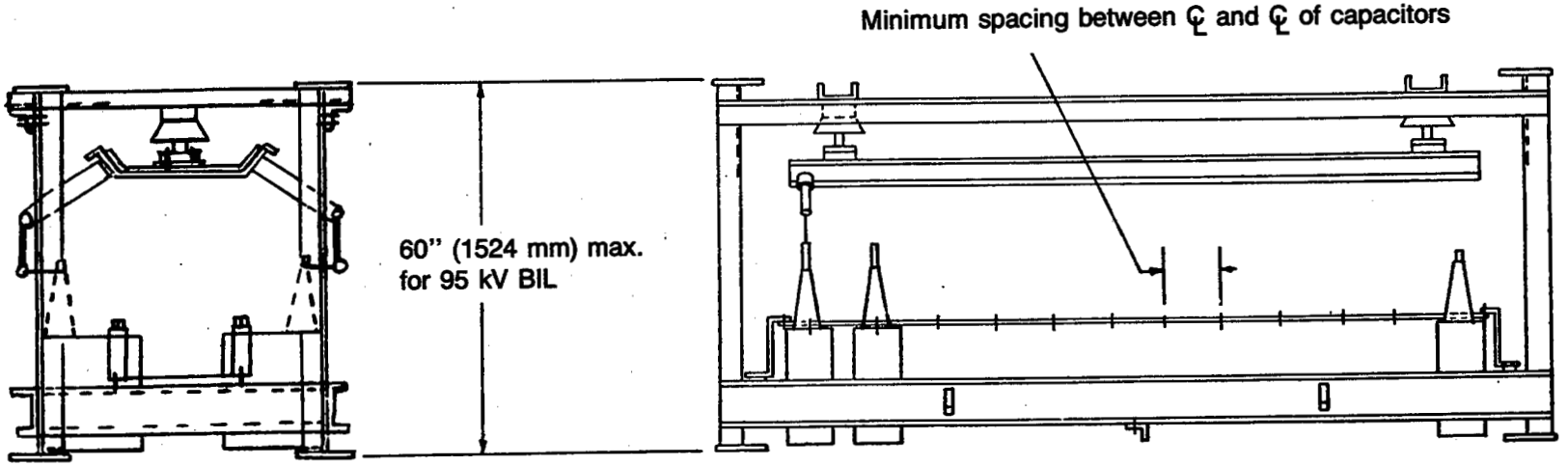
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Capacitor Rating RMS Voltage	Minimum Spacing Between Center-line to Center Line of Capacitors
2,400 - 8,000	8 inch (203.2 mm)
8,001 - 15,000	9 inch (228.6 mm)
15,001 - 25,000	11 inch (279.4 mm)

Four ¾" (19.1 mm) holes on 5" (127 mm) bolt circle

*Dependent upon bus connection and number of capacitors

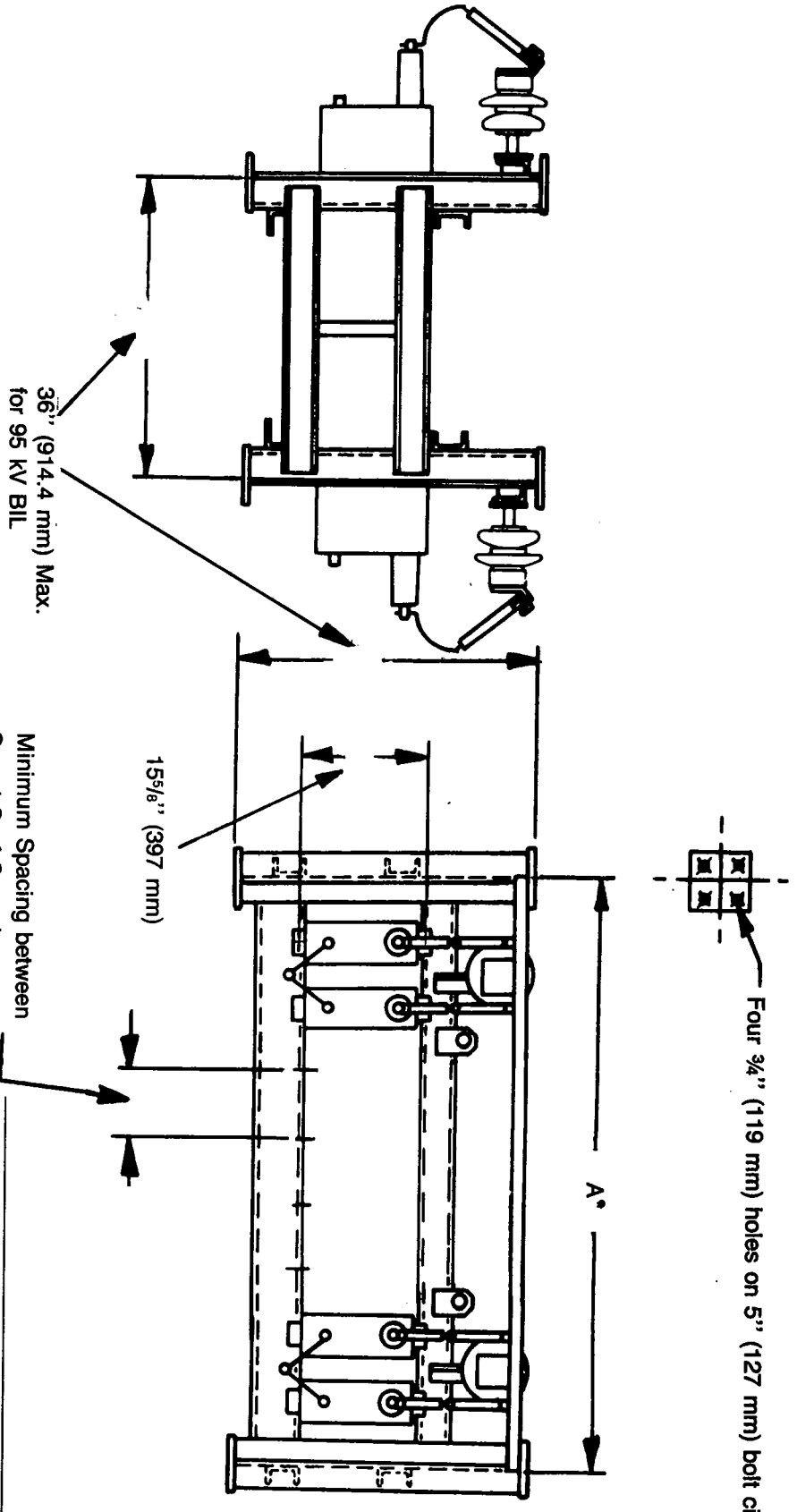


All dimensions in inches (millimeters).
Details of construction are optional.

Figure 4-1
Dimensions
Minimum Spacing Between and of Capacitors

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Capacitor Rating RMS Voltage	Minimum Spacing Between Center-line to Center Line of Capacitors
2,400 - 8,000	8 inch (203.2 mm)
8,001 - 15,000	9 inch (228.6 mm)
15,001 - 25,000	11 inch (279. mm)

*Dependent upon bus connection and number of capacitors

All dimensions in inches (millimeters).
Details of construction are optional.

Figure 4-2
Dimensions
Minimum Spacing Between and of Capacitors

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4.4.3 Horizontal Non-Enclosed Substation Equipment

Horizontal non-enclosed substation equipment using 50 kvar, 100 kvar, 150 kvar, 200 kvar, 300 kvar, and 400 kvar single-phase capacitors shall be as shown in Figure 4-2.

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4.5 NAMEPLATE MARKING FOR CAPACITORS

The following minimum amount of information shall be given on all nameplates for capacitors:

1. Name of manufacturer;
2. Identification number or type, model, style, or catalog number;
3. Rated kvar;
4. Number of phases;*
5. Rated voltage rms;*
6. Rated frequency;
7. Basic impulse level (see 5.5);
8. Amount of insulating liquid contained if flammable;†
9. Statement as to whether or not capacitors have a discharge device inside the case;
10. Year of manufacturer;
11. Unique serial number (on capacitors rated above 5 kvar) unless the number is indelibly stamped into the case; and
12. Impregnated identification. Additional marking (decal or stick-on label) shall be visible from the ground. Blue color shall be used to designate non-PCB.

NEMA Standard 11-17-1988.

*For Y-connected capacitors, indicate whether neutral is grounded. For example, 4160 GrdY/2400.

Authorized Engineering Information 11-17-1988.

†This information is necessary when capacitors are to be installed under conditions to which the *National Electrical Code* applies.

Authorized Engineering Information 11-17-1988.

4.6 NAMEPLATE MARKING FOR RACKS AND HOUSINGS OR CAPACITOR EQUIPMENTS

The following minimum amount of information shall be given on all nameplates for racks and housings or capacitor equipments:

1. Name of manufacturer;
2. Identification number or type, model, style, or catalog number;
3. Rated kvar;
4. Number of phases and connections;
5. Rated voltage; and
6. Rated frequency.

NEMA Standard 11-17-1988.

4.7 FUSES FOR RACK EQUIPMENT

The voltage rating of the individual fuses used in rack equipment shall be equal to or greater than the rated voltage of the capacitors. The current rating shall be at least 135 percent of the rated current of the capacitors.

Fuses shall have an adequate interrupting capacity for the system to which they are to be applied, except when the capacitor bank has a floating neutral or fault current is limited to a lower value, or both.

NEMA Standard 11-17-1988.

4.8 CAPACITOR BUSHINGS

The bushings of outdoor capacitors shall have the characteristics as shown in Table 4-2.

NEMA Standard 11-17-1988.

4.8.1 Operation

Bushings shall be suitable for operation at altitudes up to 6,000 feet (1,800 meters) above sea level (See 4.7).

NEMA Standard 11-17-1988.

4.8.2 Test Conditions

4.8.2.1 Test Procedure

Bushings shall be tested in accordance with the procedure described in ANSI C76.1.

4.8.2.2 Standard Conditions

Standard atmospheric and precipitation conditions shall be:

Air temperature	25°C
Barometric pressure	29.92 inches (760 mm) of mercury
Humidity-vapor pressure	0.6085 inches (15.46 mm) of mercury
Water resistivity	7,000 ohms per cube, minimum
Rate of precipitation	0.2 inch (5.08 mm) per minute
Angle of precipatation	45 degrees

4.8.2.3 Correction Factor (D) for Variation in Air Density

The air temperature at the time of the test shall be between 50°F and 104°F (10°C and 40°C).

The correction factor for the variation in air density is determined as follows:

$$D = \frac{18\,B}{459 + F}$$

Where:

D = Correction factor;

B = Barometric pressure in inches of mercury;

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F = Temperature in degrees Fahrenheit.

This correction is applicable (standard test voltage multiplied by D) only on the 60 Hz wet and impulse withstand test.

4.8.2.4 Correction Factor (H) for Variation in Vapor Pressure

Humidity—For 60 Hz dry 1-minute withstand tests and for 60 Hz wet withstand tests, no correction shall be made for variation in humidity.

For impulse withstand tests, the applied voltage shall be the standard voltage divided by the humidity correction factor in Table 4-3.

NEMA Standard 11-17-1988.

The vapor pressure at the time of test should be between 0.3 inch (7.62 mm) and 0.7 inch (17.78 mm) of mercury.

Authorized Engineering Information 11-17-1988.

4.8.3 Voltage Measurements

The 50 or 60 Hz withstand test voltage shall be applied under the conditions given in ANSI C76.1, and shall not cause any flashover.

The impulse withstand test voltage shall be applied three times under the conditions specified. If any one but not more than one of these three applications causes flashover, three additional impulses shall be applied. If flashover does not occur, the bushings shall be considered as having met the test.

NEMA Standard 11-17-1988.

4.9 CIRCUIT BREAKERS, CONTACTORS, AND DISCONNECTING DEVICES

Circuit breakers or contactors for use with capacitors may be supplied:

1. As a separate item;
2. As a part of the capacitor equipment; and/or
3. As a part of or an addition to existing metal-clad switchgear.

Authorized Engineering Information 11-17-1988.

Table 4-3
Humidity Correction Factors

Vapor Pressure Inches of Mercury	Humidity Correction Factor
0.0 (0.0 mm)	1.153
0.1 (2.5 mm)	1.127
0.2 (5.0 mm)	1.100
0.3 (7.6 mm)	1.075
0.4 (10.1 mm)	1.050
0.5 (12.7 mm)	1.025
0.6 (15.2 mm)	1.000
0.7 (17.7 mm)	0.981
0.8 (20.3 mm)	0.961
0.9 (22.8 mm)	0.941
1.0 (25.4 mm)	0.929

Table 4-2
Bushing Characteristics

Range of Capacitor Voltage Ratings (Terminal-to-Terminal) Volts, rms	Minimum Insulation Creepage Distance Inches*	60 Hz Dry 1 Minute kV rms	60 Hz Wet 10 Seconds, kV rms	Impulse 1.2 × 50 (or 1.5 × 40) Full Wave kV Crest
216-1,199	2 (50.8 mm)	10	6	30†
1,200-5,000	5½ (139.7 mm)	27	24	75
5,001-15,000	10 (254.0 mm)	35	30	95
13,200-25,000	16 (406.4 mm)	42	36	125
15,000-25,000	17 (431.8 mm)	60	50	150
19,920-25,000	26 (660.4 mm)	80	75	200

Withstand test voltages are for standard temperature and humidity at mean sea level.

*At elevations higher than 6,000 ft. (1,800 m) above sea level, additional insulation may be required to prevent bushing flashovers or excessive leakage current.

†Not applicable to indoor ratings.

(These notes have been approved as Authorized Engineering Information.)

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4.9.1 Standards

Contactors rated 600 V and less shall be in accordance with the applicable provisions of Part 2-211 of NEMA Standards Publication ICS 2.

For application information on molded case circuit breakers and other standard information, the manufacturer shall be consulted.

NEMA Standard 11-17-1988.

4.9.2 Ratings

Circuit breakers, disconnecting devices, and all current-carrying parts shall have a voltage rating adequate for the circuit to which they are to be applied. The current rating shall be at least 135 percent of the rated current of the capacitor, except that fusible safety switches shall have a current rating that is at least 165 percent of the rated capacitor current. The momentary rating of the switching device shall be sufficient for fault or inrush current and the interrupting rating, if required, shall be sufficient to handle the short-circuit duty of the system.

Where the operating current exceeds 135 percent of rated current due to harmonic components, service conditions shall permit the selection of circuit breakers and disconnecting devices with higher current ratings.

When supplied as a part of the capacitor equipment, the cables or bus work connecting the circuit breaker, contactor, or disconnecting devices to the power entrance terminals and to the capacitor rack bus work shall have a momentary rating equal to that of the switching device.

NEMA Standard 11-17-1988.

4.9.3 Application

When mounted separately from the capacitor equipment, circuit breakers and disconnecting devices shall take into consideration the special duty requirements of capacitor service.

When mounted as a part of the capacitor equipment, disconnecting devices shall have adequate clearances between live parts and the grounded structure.

Automatic circuit breakers shall be provided with three overcurrent trips (two for two-phase), one for each phase line. Sufficient time delay or range of setting shall be available in the overcurrent tripping means to avoid tripping due to capacitor inrush current. Tripping current transformers shall have a current rating equal to at least 135 percent of rated current of the capacitor and a momentary rating equal to at least 160 percent of the interrupting capacity of the circuit breaker.

NEMA Standard 11-17-1988.

4.10 AUTOMATIC SWITCHING OF CAPACITORS

4.10.1 Control

The control will normally consist of the master element, time-delay relays, and the necessary auxiliary devices.

Time-delay relays should allow sufficient time to prevent unnecessary switching operations due to momentary disturbances on the power circuit.

Such a control normally includes control switches to permit the opening and closing of each capacitor switch by manual operation of its control switch or to have the capacitor switches open and close in response to the master element. This control may be supplied in the following arrangements:

1. Separate indoor cabinet;
2. Separate outdoor cabinet;
3. With breaker or contactor in indoor cubicle;
4. With breaker or contactor in outdoor cubicle;
5. With breaker or contactor and capacitor in indoor rack or housing; or
6. With breaker or contactor and capacitor in outdoor rack or housing.

Authorized Engineering Information 11-17-1988.

For safety reasons, a fused potential transformer or control power transformer, where required, shall not be located in the low-voltage control compartment but shall be incorporated with the switch device or the capacitor or both. In all other cases, the control shall be operated from the purchaser's auxiliary power circuits. The control voltage shall be either 115 or 230 V ac. Fuse protection for this circuit shall be included.

NEMA Standard 11-17-1988.

4.10.2 Capacitor Switching Device

A capacitor switching device shall be supplied for separate mounting in a cubicle with the control or as an integral part of the capacitor. The switching device shall be selected for proper voltage, current repetitive duty, interrupting capacity, or momentary rating, or a combination of all of these. Lockout protection against reclosing on a fault shall be provided when automatic overcurrent trip is provided on the switching device.

NEMA Standard 11-17-1988.

4.10.3 Control Enclosure

If the control is included in the capacitor rack or housing, it shall be in a separate compartment or adequately barriered or metal-enclosed to protect operating personnel from the high voltages of the power circuit at all times.

NEMA Standard 11-17-1988.

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4.10.4 Voltage Control – Single-Step

Single-step voltage control shall include a voltage-sensitive relay plus time-delay and auxiliary relays that operate to open and close the capacitor switching device in response to predetermined values of circuit voltage that persist for the required time. The voltage-sensitive relay shall be adjustable over a range of 90 to 110 percent of the 115 volt base. Unless otherwise specified, the band width shall be made readily adjustable from 3 to 7½ percent.

NEMA Standard 11-17-1988.

4.10.5 Voltage Control – Multistep

Multistep voltage control shall be similar to single-step control except that it shall be arranged to switch two or more capacitors selectively and automatically in response to predetermined values of circuit voltage that persist for the required time. The voltage-sensitive relay shall be adjustable over a range of 90 to 110 percent of the 115 volt base. Unless otherwise specified, the band width shall be made readily adjustable from 20 to 7.5 percent.

NEMA Standard 11-17-1988.

4.10.6 Current Control – Single-Step

Single-step current control shall include a current-sensitive relay plus time-delay and auxiliary relays that operate to open and close the capacitor switch in response to predetermined values of load current which persist for the required time. The current-sensitive relay shall be adjustable over a range of 25 to 100 percent of the coil rating.

The current transformer for the load circuit shall not be included with the control.

NEMA Standard 11-17-1988.

4.10.7 Kilovar Control – Single-Step

Single-step kilovar control shall include a reactive kVA-sensitive relay plus time-delay and auxiliary relays which operate to open and close the capacitor switching element in response to predetermined values of kilovars which persist for the required time. The kilovar relay shall be energized from current and potential transformers. The current coils of the relay shall have continuous rating of at least 4 amperes, 60 Hz, and the potential coils shall be rated 115 V, 60 Hz.

The kilovar relay shall provide adequate adjustment when used with current transformers having a rating up to 125 percent of the maximum load and when used with voltage transformers to provide nominally 115 V for the potential winding.

Current transformers for the load circuit shall not be included in the control.

NEMA Standard 11-17-1988.

4.10.8 Kilovar Control – Multistep

Multistep kilovar control shall be similar to single-step kilovar control except that it shall be so arranged as to switch two or more capacitors selectively and automatically in response to predetermined values of desired kilovars that persist for the required time. The kilovar relay shall be energized from current and potential transformers. The current coils of the relay shall have a continuous rating of at least 4 amperes, 60 Hz, and the potential coils shall be rated 115 V, 60 Hz.

The kilovar relay shall provide adequate adjustment when used with current transformers having a rating up to 125 percent of the maximum load and when used with voltage transformers to provide nominally 115 V for the potential winding.

Current transformers for the load circuit shall not be included in the control.

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SECTION 5
TESTING STANDARDS

5.1 GENERAL

Capacitor tests are designed as either design or routine tests.

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5.1.1 Design (Type) Tests

The following design type tests shall be conducted:

1. Impulse Withstand Test (see 5.5);
2. Thermal Stability Test (see 5.6);
3. Radio Influence Voltage (see 5.7); and
4. Voltage Decay Test (see 5.8).

NEMA Standard 11-17-1988.

5.1.2 Routine (Production) Test

The following routine (production) tests shall be conducted:

1. Short-time Overvoltage Test (see 5.9);
2. Capacitance Test (see 5.10);
3. Loss Determination Test (see 5.11);
4. Discharge Resistor Test (see 5.12); and
5. Leak Test (see 5.13).

NEMA Standard 11-17-1988.

5.2 TEST CONDITIONS

Tests shall be conducted under the following conditions unless otherwise specified:

1. New and clean capacitors shall be used for each test.
2. Ambient temperature shall be 25°C±5°C.
3. All ac voltages shall have a frequency of 50 or 60 Hz and an approximately sinusoidal wave shape.

NEMA Standard 11-17-1988.

5.3 DESIGN (TYPE) TESTS

The design tests described in 5.5 through 5.8 shall be performed by the manufacturer on a sufficient number of capacitors and ratings to demonstrate compliance with these standards. These tests need not be repeated unless the design of the capacitor is changed so as to modify its performance. Capacitors shall first meet routine test requirements before being subjected to design tests.

NEMA Standard 11-17-1988.

5.4 ROUTINE (PRODUCTION) TESTS

Routine tests are tests made by the manufacturer on each capacitor to ensure that the design performance is maintained in production.

NEMA Standard 11-17-1988.

5.5 IMPULSE WITHSTAND TEST— CASE INSULATION (DESIGN TESTS)

The test capacitors shall be capable of withstanding an impulse voltage test at the voltages shown in Table 5-1.

Table 5-1
Impulse Test Voltages

Range of Capacitor Voltage Ratings (Terminal-to-Terminal) Volts, rms	Impulse Test, kV Crest
216 - 1,199	30*
1,200 - 5,000	75
5,001 - 15,000	95
13,200 - 25,000	125

* Outdoor capacitors only.

Single bushing capacitors where the case forms one electrode shall not be subjected to the impulse withstand test. When one principal terminal of the capacitor is connected to the case, the BIL requirements shall not apply to the internal insulation assembly. The internal insulation assembly shall assure that the capacitor will meet the requirements of 5.9. However, the bushing shall meet the requirements of 4.8, and the nameplate shall carry the applicable BIL.

The test shall consist of three successive 1.2 × 50 microsecond positive full-wave impulses applied between the terminals (connected together) and the case or housing. The tolerance on test waves shall be as noted in Table 5-2.

NEMA Standard 11-17-1988.

Table 5-2
Test Wave Tolerances

Quantity Measured	Tolerances on 1.2 × 50 Microsecond Impulse Wave, Percent
Crest Value	±3
Front Time	±30
Time to half value	+0. –20

5.6 THERMAL STABILITY TEST (DESIGN TEST)

The test capacitor shall be considered thermally stable if the hot spot case temperature reaches and maintains

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a constant value within a variation of 3°C for 24 hours under the test conditions described in 5.6.1 and 5.6.2.

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5.6.1 Selection of Samples

One sample shall be constructed with thermocouples positioned internally to measure the maximum dielectric temperature. Two other capacitors of the same ratings and having approximately the same power factor and capacitance (at rated voltage, rated frequency, and case and internal temperatures at ts) as the capacitor with the thermocouples shall be selected for barrier capacitors.

NEMA Standard 11-17-1988.

Resistor models having the same power loss, thermal characteristics, and physical dimensions as the test capacitor may be substituted for the barrier capacitors.

Authorized Engineering Information 11-17-1988.

5.6.2 Test Method

5.6.2.1 Mounting Conditions

The test capacitor, selected as above, shall be mounted in an enclosure between the two barrier capacitors at the manufacturer's minimum recommended center-to-center spacing. The mounting positions selected shall be the recommended operating position which produces the highest internal temperature.

NEMA Standard 11-17-1988.

5.6.2.2 Ambient Temperature

The air inside the test enclosure shall be maintained at an average temperature of 46°C and shall not be force-circulated. The inside wall temperature of the enclosure shall be within ±5°C of the ambient temperature in the enclosure.

The ambient temperature shall be measured by means of a thermocouple on the case or within the dielectric of an isolated unenergized capacitor, supported and positioned so that it is subjected to minimum possible thermal radiation from the three energized samples.

NEMA Standard 11-17-1988.

5.6.2.3 Test Voltage

All three sample capacitors shall be energized at a test voltage to be determined as follows:

$$V_T = 1.1\, V_R \times \sqrt{\frac{W_M}{W_A}}$$

Where:

V_T = Test voltage

V_R = Capacitor rated voltage rms

W_M = Manufacturer's maximum allowable power loss. This loss shall be calculated using 110 percent of rated voltage rms and the manufacturer's established maximum product of measured capacitance and power factor, at rated voltage and frequency and at a stated case and internal temperature ts.

NOTE: W_M does not correspond to an exact limit on either capacitance or power factor but does correspond to an exact limit on their products. (This sentence is classified as Authorized Engineering Information.)

W_A = Actual power loss of the test capacitor. This loss shall be calculated using 110 percent of rated voltage rms and the actual capacitance and power factor of the test capacitor measured at rated voltage and frequency and at a stated case and internal temperature ts.

t_s = Manufacturer's dielectric temperature limit under the conditions of this thermal stability test.

The test voltage (V_T) calculated for this test shall be limited to a value that will result in operation of the test capacitor at a maximum of 140 percent of its kilovar rating. This voltage shall be maintained constant, within ±2 percent throughout the last 24 hours of the test period.

NEMA Standard 11-17-1988.

5.6.2.4 Temperature Measurement

The temperature of the test capacitor shall be measured by means of thermocouples attached to the case sidewall and cover and positioned internally so as to measure the maximum dielectric temperature. All temperature measurements shall be accurate within ± 1°C.

NEMA Standard 11-17-1988.

5.7 RADIO INFLUENCE VOLTAGE (DESIGN TEST)

Radio influence voltage measurements on capacitors shall be conducted in accordance with the requirements of 5.7.1 through 5.7.5.

NEMA Standard 11-17-1988.

5.7.1 Equipment

The equipment and general method used in determining the radio influence voltage shall be in accordance with NEMA Standards Publication 107.

NEMA Standard 11-17-1988.

5.7.2 Test Voltages

Capacitors shall be tested at 115 percent of their rated voltage rms.

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5.7.3 Method of Test

Capacitors having two or more bushings with the windings fully insulated from the case shall be tested with the case grounded and with the voltage applied between all bushings connected together and the case. Capacitors having only one bushing per phase with the case as the other terminal shall not be tested. This type of construction precludes any meaningful RIV measurement due to the high capacitance.

NEMA Standard 11-17-1988.

5.7.4 Precautions in Making Tests

The following precautions shall be observed when measuring the radio influence voltage of capacitors:

1. The capacitor shall be at approximately the same temperature as the room in which the tests are made;
2. The bushings of the capacitor shall be dry and clean; and
3. The capacitor shall be mounted in its normal position with the recommended clearance.

NEMA Standard 11-17-1988.

5.7.5 RIV Limits

The radio influence voltage when measured in accordance with the foregoing at a frequency of 1 megahertz, shall not exceed 250 microvolts for all capacitors rated 25,000 V and less.

NEMA Standard 11-17-1988.

5.8 VOLTAGE DECAY TEST (DESIGN TEST)

Capacitors shall be energized at rated ac voltage rms or at a dc voltage equal to $\sqrt{2}$ times rated voltage rms. The capacitor shall then be de-energized, and the decay of the voltage shall be measured by suitable means. The time for the residual voltage to decay to 50 V or less shall not exceed 5 minutes for capacitors rated above 600 V or 1 minute for capacitors rated 600 V or less.

NEMA Standard 11-17-1988.

5.9 SHORT-TIME OVERVOLTAGE TESTS (ROUTINE TESTS)

1. Each capacitor shall withstand a sinusoidal test voltage at 50 or 60 Hz or a dc voltage for 10 seconds in accordance with the following paragraphs.
2. The voltage shall be applied in such a manner as to avoid transients. The capacitor's case and internal temperature shall be 25°C ± 5°C.

NEMA Standard 11-17-1988.

5.9.1 Terminal-to-Terminal Tests

Terminal-to-terminal tests shall be made on individual capacitors as follows:

Each capacitor shall withstand an alternating sinusoidal voltage of two times rated voltage rms or a dc voltage of 4.3 times rated voltage rms.

NEMA Standard 11-17-1988.

For those systems with higher than normal overvoltages, a special design for capacitors rated 2,400 V rms or higher may be used for which this test will be increased to a dc test voltage of 6.25 × rated voltage rms in accordance with agreement between manufacturer and purchaser.

Authorized Engineering Information 11-17-1988.

For three-phase wye connected capacitors, the above testing for terminal-to-neutral shall be followed by a test at $\sqrt{3}$ times the above values between each outside bushing to the center bushing to test the phase insulation.

The capacitance shall be measured on each capacitor both before and after the application of the test voltage. The initial capacitance measurement shall be at low voltage. The change in capacitance, as a result of the test voltage, shall be less than the value caused by failure of a single roll of the particular design.

NEMA Standard 11-17-1988.

5.9.2 Terminal-to-Case Tests

Terminal-to-case tests shall be made on individual capacitors having all terminals insulated from the case, using the ac test voltages in Table 5-3.

Table 5-3
Terminal-to-Case Test Voltages

Range of Capacitor Voltage Ratings (Terminal-to-Terminal)		Alternating-current Test Voltage (Terminal-to-case)	
Volts RMS	BIL	Indoor	Outdoor
0 - 300	30*	3,000	10,000
301 - 1,199	30*	5,000	10,000
1,200 - 5,000	75	...	26,000
5,001 - 15,000	95	...	34,000
13,200 - 25,000	125	...	40,000

*Outdoor capacitors only.

In making the foregoing terminal-to-case dielectric tests, all terminals shall be connected together and the test voltage applied from terminal to case.

For capacitors having one terminal common to the case, the foregoing terminal-to-case test voltages shall not apply, and the only test shall be the terminal-to-terminal test.

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5.10 CAPACITANCE TEST (ROUTINE TEST)

Capacitance tests shall be made at the factory to demonstrate that each individual capacitor will deliver not less than the rated kvar and not more than 115 percent of rated kvar at rated voltage and frequency, corrected to a capacitor case and internal temperature of 25°C. Capacitance measurements shall be traceable to the National Institute for Science and Technology (formerly the National Bureau of Standards.)

5.11 LOSS TEST (ROUTINE TEST)

Loss measurement shall be made by the manufacturer on each capacitor to demonstrate that the capacitor losses are equal to or less than W_M as defined in 5.6.

NEMA Standard 11-17-1988.

5.12 DISCHARGE RESISTOR TEST (ROUTINE TEST)

Each capacitor containing an internal discharge resistor shall be tested after the terminal-to-terminal potential test to ensure that the resistors are within design limits sufficient to meet the requirements (5.9.1). The value shall be permitted to be determined at a low voltage using a suitable resistance bridge.

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5.13 LEAK TEST (ROUTINE TEST)

A suitable leak test shall be made to demonstrate that each capacitor is free from leaks.

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SECTION 6
GUIDE FOR THE APPLICATION AND OPERATION OF SHUNT CAPACITORS

6.1 GENERAL

The manufacturer's instructions should be carefully studied and followed in order to secure the best results. It is impossible to cover here in detail the complete rules for the installation of each of the different types of capacitors manufactured, but the following information is given relative to the most important points to be considered.

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6.2 RELIABILITY

The reliability of capacitors should typically generate a failure rate of less than 0.5 percent for the first year with lower rates in following years until ultimate wearout occurs.

The life of a capacitor is shortened by overstressing, overheating, chemical change, physical damage, or repeated temperature changes. Therefore, the length of life depends upon the control of operating conditions involving voltage, temperature limits, and physical care.

Authorized Engineering Information 11-17-1988.

6.3 OVERVOLTAGE LIMITS AND PROTECTION

Capacitors cause a voltage rise at the point where they are located; thus, the operating voltage is increased. Capacitors are, therefore, more likely to operate at overvoltages than other types of equipment that cause a voltage drop at the point where they are located. Because of this factor, the nameplate voltage rating of capacitors and permissible overvoltage operation are higher than those established for most other circuit devices, such as motors. For example, a motor rated 440 V is recommended for operation on the same circuit as a capacitor rated 480 V. Standards have been established to allow capacitors to operate at 110 percent of rated voltage rms, provided that the crest voltage including all harmonics does not exceed $1.2 \times \sqrt{2}$ times rated voltage rms and provided that the maximum permissible 1.35 times rated kvar is not exceeded. If the 110 percent voltage is exceeded, then the circuit voltage should be reduced, the capacitors switched off during the high-voltage periods, or capacitors with higher voltage ratings used. Daily operation at the upper voltage limit and temperature limits will shorten the life of capacitors, and such operation should be permitted only in cases of emergency.

Capacitors are frequently connected directly in parallel with induction motors and switched by means of a motor switching device. Overvoltage may result when the motor capacitor combination is disconnected from the line, since the inertia of the motor and its mechanical load will keep the motor rotating and the motor will operate as an induction generator. The voltage of self-excitation for a given motor and capacitor combination will depend upon the intersection of the capacitor volt-ampere line and the motor magnetization curve. To ensure against such overvoltages, the electrical size of capacitors should be limited to the no-load reactive component of the motor.

When a capacitor larger than permitted above is used, a separate switch, controlled by the motor switch, to automatically disconnect the capacitor when the motor is disconnected is recommended.

When a motor can be rapidly de-energized and re-energized, the possibility of high transient torques should be considered. Capacitors switched with motors prolong the duration of residual voltage in the motor as it comes to rest after de-energization. In cases where motors and capacitors are to be rapidly de-energized and re-energized, the motor manufacturer should be consulted.

Capacitors may be operated above 110 percent of rated voltage under emergency and infrequent conditions. The magnitude of the overvoltages that may be tolerated without loss of life is dependent upon the duration of each overvoltage, the number of applications, and the temperature of the capacitor. The values shown in Table 6-1 are based on full life expectancy when the overvoltages are limited to a combined total of 300 applications during the life of the capacitor. In addition, the limitations shown in Table 6-1 are based on the occurrence of overvoltages when internal temperatures of the capacitors are less than 0°C. The multiplying factors shown in these tables may be increased, upon recommendation by the manufacturer, when fewer overvoltages are expected or when less severe temperature conditions exist.

Table 6-1
Maximum Momentary Overvoltage Limits

Duration	Multiplying Factor Times Rated Rms Voltages
15 cycles	2.0
1 second	1.7
15 seconds	1.4
1 minute	1.3
30 minutes	1.25

The overvoltage limits apply for power frequencies where high frequency transients are not superimposed.

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The crest voltage should not exceed $\sqrt{2}$ times the foregoing rms values.

High voltage and current transients are uncommon in most power circuits, but capacitors may be subjected to both high voltage and high current under certain conditions associated with switching. The magnitude of the permissible current and voltage peaks depends on the frequency of occurrence. In the case of a frequently switched capacitor, current and voltage peaks should be held to lower values, whereas higher values may be tolerated occasionally.

1. A capacitor reasonably may be expected to withstand peak transient currents of up to 1,000 times rated current rms twice per year and up to 100 times rated current rms 1,000 times per year.
2. A capacitor reasonably may be expected to withstand the transient overvoltages listed in Table 6-2.

Table 6-2
Transient Overvoltage Withstand Capability

Probable Number of Transients Per Year	Multiplying Factor to be Applied to Rated Voltage rms
40	4.0
400	3.4
4,000	2.9

Capacitors connected to exposed lines may require surge protection by station-type of line-type surge arrestors as close as possible to the capacitor. If capacitors are located indoors, the arrestors may be located at the line entrance to the building. Capacitors connected between the line and grounded neutral may be effective in reducing the slope of a travelling wave front but, since the available energy sometimes may be sufficient to charge the capacitors to a dangerously high voltage, an arrester arranged in parallel with the capacitors is recommended for protection.

Capacitor banks installed on three-phase, four-wire, multi-grounded neutral distribution feeder circuits frequently are connected in wye with the neutral of the capacitor bank connected to the system multi-grounded neutral conductor. Under certain conditions, the neutral of the capacitor bank may be disconnected from the system neutral conductor to reduce the harmonic currents in the system. With the neutral of the capacitor bank floating to reduce harmonic currents, or if the bank is normally installed in the ungrounded wye configuration, a fault in one phase of the bank may subject the capacitors in the unfaulted phases to overvoltage. A completely faulted phase of a capacitor bank may subject the capacitors in the unfaulted phases to $\sqrt{3}$ times system line-neutral voltage. With fusing practices, the time that the capacitors are subjected to the overvoltage may exceed the stated overvoltage capability of the capacitor as defined in Table 6-2. The user should recognize that sustained high overvoltage may be impressed on capacitors in ungrounded wye capacitor banks if capacitor switches and unbalanced detection schemes are not used.

Fuses are not recommended for use in series with discharge devices, including potential transformers or reactors. If fuses are used, their current-carrying capacity should be sufficient to carry the capacitor discharge current without damage and should be of the indicating type.

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6.4 OPERATING AND AMBIENT TEMPERATURES

It is essential that consideration be given to the arrangement of capacitors and complete equipment as an installation to provide adequate ventilation and dissipation of losses. Capacitors may be designed to operate at a lower temperature rise than most other types of apparatus for the following specific reasons:

1. Capacitors may operate at full load continuously, which eliminates the benefit of an average temperature rise derived from the usual load cycle under which most other apparatus operate.
2. Capacitors may be designed to operate at comparatively high dielectric stresses for reasons of economy. The combination of these stresses with operation at high temperature for extensive periods of time may result in gradual deterioration and shortened life.

Capacitor ratings are based on maximum ambient temperatures with an allowance for heat dissipation by radiation and convection. The arrangement and mounting of units and the conditions of installation may affect the heat dissipation and thereby limit the ambient temperature at which the capacitor may be operated. The following points are important in relating the operating temperature of a capacitor to the conditions of installation:

1. An individual non-enclosed capacitor, such as is mounted on a pole outdoors, may dissipate losses with the least temperature rise (the heat dissipation being approximately 45 percent by radiation and 55 percent by convection).
2. The mounting of capacitors in rows side by side or in tiers, or both, may increase the temperature rise in each tier above the tier below because of heating of the air stream and because of reduced radiation.
3. The enclosing of capacitors is a housing or room may increase the temperature rise because of reduced radiation and restriction of the natural circulation of air.

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4. Capacitors subjected to radiation from the sun or from any surface, the temperature of which is above the ambient, may show a higher temperature rise.
5. Capacitors and equipments operating outdoors without restriction on movement of air normally may operate with lower temperature rises than those operating indoors in still air conditions. This reduction in temperature rise will usually more than offset any additional temperature rise due to direct radiation from the sun.

Indoor installations may require special consideration due to possible continuous high ambient temperatures and restricted air movement.

Individual capacitors rated 600 V and below, installed indoors without enclosures or restricted ventilation (live terminal parts and fuse connections may be enclosed with an allowance for the free circulation of air about the sides other then the top), may be suitable for continuous operation at ambient temperatures up to and including 46°C. Where ambient air temperatures higher than listed in 2.3 are expected in service, the manufacturer's recommendations should be sought.

There is a risk of damage to capacitors if they are energized when their temperature is below the minimum of –40°C cited in 2.3.2. The manufacturer's recommendation should be sought when energization at temperatures below this minimum is considered.

The use of a discharge device is intended to supplement rather than displace the short-circuiting of a capacitor before handling.

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6.5 ABNORMAL OVERLOAD CURRENT

Overload capacitor currents caused by excessive fundamental voltages or harmonic voltages may occasionally be encountered. Total rms currents due to fundamental and harmonic voltage should be limited to a maximum of 1.8 times the normal 50 to 60 Hz rating of capacitors rated 2,400 V or higher. The blowing of fuses or excessive temperature rise, or both, may be the first noticeable indication of an overload condition.

Capacitors and auxiliary devices are designed for continuous operation up to 1.35 times rated kilovar including the kilovar due to the fundamental voltage and all harmonic voltages provided that the capacitor voltage does not exceed an rms value of 1.1 times rated or a peak value of $1.2\times \sqrt{2}$ times rated voltage rms. When one harmonic voltage predominates (as is usually the case), Figure 1 in ANSI C55.1 offers a convenient means for determining the total capacitor current (fundamental plus harmonics) that can be tolerated without exceeding the kilovar and voltage limitations. Where currents with substantial harmonic components are likely to be encountered, provision should be made for additional current-carrying capacity in the circuit breakers, fuses, and other auxiliary devices.

If harmonic currents are above the allowable limits, one or more of the following remedies should be undertaken.

1. Relocation of the capacitors to other parts of the circuit may reduce overcurrent due to partial resonance.
2. Capacitors may be switched off the circuit during periods in which overcurrents are likely to occur. Automatic control actuated by change, in current, change in voltage, change in reactive kVA, or by time clock may be used.
3. The neutral ground, if present, may be removed. It should be noted that bank insulation and switch load interrupting rating may be inadequate if neutral is disconnected.
4. If these remedies fail, it may be necessary to resort to the use of reactors of a selected rating. These may be connected in series or shunt with all or a part of the capacitor bank to reduce the harmonic current. The use of reactors necessitates the determination of the exact harmonic causing excessive current, which may be done with a harmonic voltmeter, oscillograph, or harmonic analyzer. Careful consideration should be given to allowing for increased voltage or current loading on a capacitor as the result of adding a reactor.

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6.6 INSPECTION AND MAINTENANCE

Inspection should be made within 8 to 24 hours after the installation of capacitors and during the first periods of light load on the circuit when maximum overvoltage will be obtained. It is recommended that at least 5 minutes be allowed to discharge and then to short-circuit the capacitor unit terminals together and to ground before touching any live parts. Readings of voltage and current in each phase should be made to determine that:

1. Phase voltages are balanced within the limits of the capacitor rating; and
2. Operating kilovar (that is, the sum of the fundamental frequency kilovar and any harmonic frequency kilovar that may be present) does not exceed 135 percent of the rated value.

Regular inspection of the capacitor installation on an established schedule should include a check of ventilation, fuses, temperature, and voltage conditions. Capacitor bushings and insulating surfaces should be cleaned periodically, depending on the severity of conditions to which the insulators are exposed. Capacitors or equipment exposed to weathering should be repainted periodically to prevent excessive corrosion.

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Handling and disposal of capacitor insulating fluid should follow the methods prescribed by the Environmental Protection Agency or other governing agencies.

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6.7 FIELD TEST ON CAPACITORS

Field tests on capacitors may include voltage test for insulation strength (both line-to-line and line-to-case), capacitance or current test, insulation resistance test, power factor or loss measurement, and seal test for liquid tightness.

Tests may be divided into two classes, as shown in 6.7.1 and 6.7.2.

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CAUTION: Capacitors may rupture during the tests in 6.7.1 and 6.7.2. Adequate safeguards should be provided to prevent injury to personnel or damage to adjacent equipment in event of violent failure of a capacitor during test. Testing should be done at or near room temperature to avoid damage to the dielectric. The capacitor may be damaged if discharged by short-circuiting its terminals before five minutes after the test potential is removed. Before any tests are initiated, the manufacturer's instructions should be carefully studied and followed.

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6.7.1 Tests on Capacitors Before Placement in Service

Tests on new capacitors may be made using voltages not exceeding 75 percent of the routine test voltage given in 5.9. Experience has shown that these tests are not necessary on all capacitors. In applying low-frequency tests, it is recommended that the capacitor be energized at a voltage not in excess of the nameplate rating, and then that the voltage be raised to 75 percent of the factory test value. To de-energize the capacitor, the voltage should be reduced to a value not in excess of rated voltage before opening the circuit.

It may be more convenient to use direct current in testing. Again, the line-to-line test should be made at a voltage not exceeding 75 percent of the dc routine test voltage given in 5.9. The duration of this test, including time to charge the capacitor up to the required value, should not exceed 15 seconds to avoid the possibility of damaging built-in discharge resistors.

The dc test voltages shown in Table 6-3 are for capacitors with all terminals isolated from the case and should be applied from short-circuited terminals to case.

Table 6-3
DC Field Test Voltages

Rated Voltage of Capacitors Volts	Impulse Test, kV Crest	DC Field Test Voltage, Volts Terminal-to-Case
216-1,199	30†	15,000*
1,200-5,000	75	28,500
5,001-15,000	95	39,000
13,200-25,000	125	45,000

*For indoor units, only 7,500 volts should be used.

†For outdoor units only.

In dc testing, the charging rate should be limited to a value not in excess of one ampere. Hence, a resistor having a resistance in ohms not less than the value of the testing potential in volts should be connected in series with the capacitor. A 50-watt resistor rating will be satisfactory. A similar resistor of 50,000 to 100,000 ohms should be connected across the capacitor to drain the charge after the testing potential is removed.

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6.7.2 Tests on Capacitors After Placement in Service

Field tests may be made to ascertain the operating condition of a capacitor. Such tests are recommended only in the case of indication of trouble or after exposure to possible damage. The serviceability of a capacitor may be determined by one or more of the following simple tests.

1. The condition and insulation strength of the line-to-line dielectric or between shorted line terminals and the case may be tested by applying an overvoltage not exceeding 75 percent of the routine test voltage given in 5.9.

   For the test procedure, reference should be made to the recommendations given in 6.7.1.
2. Capacitance may be determined by utilizing a lso voltage capacitance meter. Capacitance also may be determined by measuring the current while applying a known voltage and frequency (preferably rated voltage and frequency) of a reasonably good wave shape. These tests also generally will indicate a short-circuited capacitor or open-circuited capacitor. See 3.1 and nameplate rating for the determination of nominal capacitance values.
3. Line-to-line internal discharge resistor may be checked with a suitable bridge or calculated from the dc voltage and current readings.
4. Measuring line-to-line power factor or dielectric loss provides a means of determining the operat-

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ing condition of the dielectric. Such loss measurements should be made at rated frequency and at test voltages not less than 25 percent of rated voltage to obtain accurate results.

5. Line-to-case insulation resistance measurements may be made to determine the condition of the line insulating terminals and dielectric insulation to case. The resistance measured should be not less than 1,000 megohms. This test is not applicable to single bushing capacitors. Measuring the line-to-case power factor or dielectric loss is another means of determining the condition of the line insulating terminals and insulation to case, but it has no advantage over the resistance test described.
6. Liquid tightness of a capacitor may be checked by increasing the internal pressure and inspecting for leaks. This may be done effectively by thoroughly cleaning the case, heating the capacitor a minimum of four hours in an oven, and then placing it horizontally on clean paper with the suspected point of leakage on the bottom. The temperatures of the capacitor case should not be allowed to exceed the manufacturer's recommendations; 50°C may be used if the manufacturer's limit is not available.

The measurable characteristics of properly applied and installed capacitors that are hermetically sealed are not expected to change with time. Therefore, periodic testing may not be necessary. However, operating conditions may change, resulting in damage and short life; hence, periodic inspection and check of such operating conditions as outlined previously in this section are highly desirable.

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6.8 FUSING GUIDELINES

6.8.1 General

Since capacitors contain large areas of insulation that are operated at relatively high-voltage stress, some insulation failures should be expected. The system fault current available at the capacitor location, type of connections, such as delta or wye, neutral grounded or ungrounded, kvar rating of the individual capacitors and the bank, and the number of capacitors in parallel, are factors that should be considered when determining the proper protection for a capacitor bank. A properly applied protection scheme should minimize the probability of capacitor case rupture.

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6.8.2 Fuse Current Rating

The current rating of the expulsion fuse link or the current-limiting fuse will exceed the rated current of the capacitor by a factor. This factor is based on the type of bank, its connections, and variations that can occur, such as capacitor tolerances, over-voltage operation, and harmonics. Care should be exercised in the selection of the factor since a fuse that is too large increases the probability of a case-rupture occurrence, and a fuse that is too small will cause unwanted fuse operation. The selection of a proper fuse balances these two parameters.

In general, the smallest fuse that has adequate capacity to withstand the transient currents that can occur and will continuously carry the maximum current expected at the capacitor bank location will be the best selection.

Current-limiting fuses often have de-rating factors that need to be applied to the current rating due to the applications environment. Expulsion fuse links also could have de-rating factors for environmental conditions. However, many types of expulsion fuse links have continuous-current-carrying capabilities that exceed their rating.

The fuse manufacturer should be consulted if any of the facts necessary for application are unknown on any particular device.

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6.8.3 Fuse Voltage Rating

The voltage rating of fuses used for individually fused capacitors should be equal to, or greater than, the nameplate voltage rating of the capacitors. For group fusing of capacitors, the voltage rating should be equal to, or greater than, the system voltage. If the bank's neutral is solidly grounded and no physical conditions exist that can impose line-to-line voltage across the fuse during a fault, then a line-to-neutral rated fuse may be used. If the fuse is a current-limiting type, the lowest voltage rating that exceeds the capacitor voltage rating should be used since use of a current-limiting device having too high a voltage rating could produce undesirable high peak arc voltages, which, in turn, impose high voltage transients on the power system.

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6.8.4 Fuse Interrupting Rating

All fuses should have an interrupting rating that exceeds the available fault current to which the fuse may be subjected. The fault currents may be limited by current-limiting reactors, multiple series capacitors, a floating neutral, or other means.

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6.8.5 Stored-Energy Transients

Stored-energy transients are a concern for fuses used with individual capacitor units.

Proper selection of the fuse should take into account the energy stored in a parallel-connected group of

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capacitors. If a capacitor-unit failure occurs, the energy stored in each parallel-connected capacitor will discharge through its own fuse. Fuse selection should be made so that it can withstand the I^2T of this high-frequency discharge.

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The discharge from all of the parallel-connected capacitors will flow through the failed capacitor and its fuse. The fuse shall have a Joules-interrupting rating that exceeds the maximum parallel-connected energy expected, considering all voltage conditions that can exist.

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When individual expulsion-type fuses are used, in order to minimize the probability of failure of the expulsion fuse or rupture of the capacitor case, the total energy stored in a parallel-connected group of all-film capacitors should not exceed 15,000 Joules when computed on the basis of the peak capacitor voltage being $1.1\sqrt{2}$ times rated voltage rms; for 60 Hz applications, 4,650 kvar at rated voltage is recommended as the limit for maximum parallel-connected kvar. Exposure to higher "allowable" overvoltages may indicate the desirability of further reduction in the number of parallel-connected all-film capacitors, retaining the maximum parallel-connected energy of 15,000 Joules on the basis of the higher voltage.

When the capacitor dielectric is all paper or paper-film, the parallel energy should not exceed 10,000 joules, or, at 60 Hz, 3,100 kvar at rated voltage for maximum parallel-connected kvar.

When higher energy levels of parallel-connected capacitors are encountered, current-limiting fuses or other suitable devices or connection schemes may be required to avoid discharge of excessive energy into the faulted capacitor.

Installation procedures for fuses and selection and maintenance of switches and other protective or switching equipment is extremely important since restrictions caused by these devices can significantly increase the energy stored in the parallel units.

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6.8.6 Capacitor Protection Schemes

The two most commonly used protective schemes are primary group fusing and individual capacitor fusing.

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6.8.6.1 Group Fusing

Group fusing is more often used on small distribution banks. Rating of group fuses should be selected which will:

1. Withstand the inrush current during energization;
2. Carry the continuous bank current with adequate allowance for normal overloads caused by voltage regulation, harmonics, plus tolerances in capacitance; and
3. Where possible, isolate a capacitor-unit internal fault before the internal gas pressure causes rupture of the failed unit and, in the case of ungrounded wye-banks, before the remaining capacitors in the unfaulted phases are damaged by overvoltages.

Where only group fusing is used, it is important that the fuse have a time-current clearing characteristic consistent with the degree of risk, associated with case rupture, that will be acceptable for the type of installation and location contemplated.

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6.8.6.2 Individual Fuses

Individual capacitor fuses are commonly used on relatively large capacitor banks. In general, the operation of the fuse in banks involving more than one series group per phase, and in all ungrounded wye-banks irrespective of the number of series groups per phase, will increase the voltage on the capacitors remaining in service in that series group. The protective scheme should include provision for disconnecting the entire bank before the voltage on the remaining capacitors exceeds the values recommended in 6.3.

To prevent involvement of adjacent parallel capacitors and/or fuses in the fault when individual fuses are used, the following conditions should be considered:

1. The fuses and capacitors need to be properly spaced;
2. Any exhaust gases from the fuses should be properly directed or controlled; and
3. The correct installation procedures used for the fuse leader is so that its motion and position is controlled.

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6.8.7 Maximum Fault Currents

It is recommended that any inductive fault current flowing through a capacitor be limited to 4,000 amperes rms for 25 through 150 kvar capacitors and 5,000 amperes rms for 200 kvar and larger capacitors. If higher system fault currents are available, the use of current-limiting fuses should be considered. The fuse and capacitor manufacturers may be consulted if these conditions exist.

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6.8.8 Recommendations

Typical curves indicating regions of high and low probabilities of case ruptures for capacitors with paper, paper-film or all-film dielectrics are illustrated in Figure 6-1.

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At the request of the user, the capacitor manufacturer should provide the user with case-rupture curves for their capacitors.

At the request of the user, the fuse manufacturer should provide the fuse data necessary for application of fuses to capacitors.

If the fuse has operated, the capacitor associated with that fuse operation should be checked for proper capacitance before re-fusing and re-energizing.

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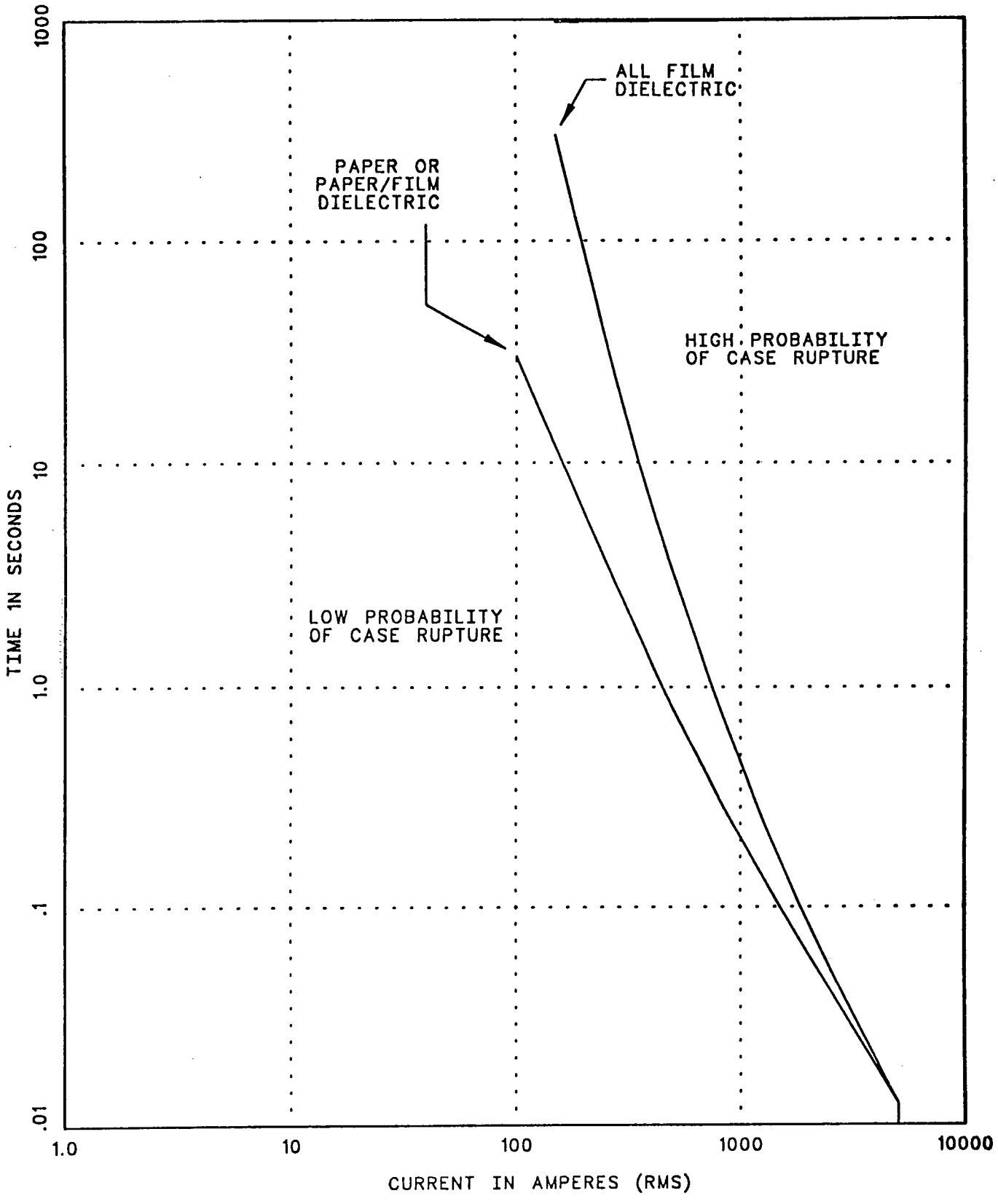


Figure 6-1
Typical Case Rupture Curves for Approximately 1800 in³ Case Volume

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NEMA STANDARDIZATION

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National Electrical Manufacturers Association Standards are adopted in the public interest and are designed to eliminate misunderstandings between the manufacturer and the purchaser and to assist the purchaser in selecting and obtaining the proper product for its particular need. Existence of a National Electrical Manufacturers Association Standard does not in any respect preclude any member or nonmember from manufacturing or selling products not conforming to the standard. *(Standardization Policies and Procedures, p. 1)*

Definition of a Standard

A standard of the National Electrical Manufacturers Association defines a product, process, or procedure with reference to one or more of the following: nomenclature, composition, construction, dimensions, tolerances, safety, operating characteristics, performance, rating, testing, and the service for which they are designed.
(Standardization Policies and Procedures, p. 2)

Dimensions

Where dimensions are given for interchangeability purposes, alternate dimensions satisfying the other provisions of the standards publication may be capable of otherwise equivalent performance.
(Standardization Policies and Procedures, p. 9)

Classes of Standards

National Electrical Manufacturers Association Standards are of two classes:

1. NEMA Standard, which relates to a product commercially standardized and subject to repetitive manufacture, which standard has been approved by at least 90 percent of the members of the Subdivision eligible to vote thereon;
2. Suggested Standard for Future Design, which may not have been regularly applied to a commercial product, but which suggests a sound engineering approach to future development, which standard has been approved by at least two-thirds of the members of the Subdivision eligible to vote thereon.

(Standardization Policies and Procedures, pp. 8 & 17)

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(Standardization Policies and Procedures, pp. 8 & 17)

Official Standards Proposal

An Official Standards Proposal is an official draft of a proposed standard which is formally recommended to an outside organization(s) for consideration, comment, and/or approval, and which has been approved by at least 90 percent of the members of the Subdivision eligible to vote thereon.
(Standardization Policies and Procedures, pp. 8 & 17)

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Standards in NEMA Standards Publications are identified in the foreword or following each standard as "NEMA Standard" or "Suggested Standard for Future Design." These indicate the status of the standard. These words are followed by a date which indicates when the standard was adopted in its present form by the Association.

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